

# Universal dynamics of pore formation in membranes.

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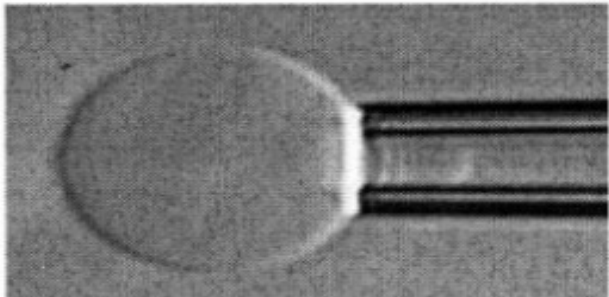
<sup>1</sup>Collaboration with D.J.Bicout.

**Fluid membranes are indispensable constituents of all living things ( $\simeq 200 \text{ km}^2$  in a human body). They are made of self-assembling amphiphilic molecules, mostly lipids, which aggregate to bilayer sheets in an aqueous environment.**

- "The entire preoccupation of a physicist is with things that contain within themselves a principle of movement and rest", Aristotle (340 BC).
- Pores in membranes are such things !

# **INTRODUCTION on DTS TECHNIQUE.**

# Image of a 20 – *mm* vesicle aspirated in a micropipette



# DTS experiments may be easy to conduct but difficult to interpret

- Rupture tests on different types of giant lipid vesicles.
- Loading rate from 0.01 and up to 100 ( $mN/m$ )/s.
- Output : (i) rate of membrane rupture ; (ii) distributions of breakage tensions governed by the kinetic process of membrane failure.
- One might naively expect that lipid membranes will rupture at tensions close to the hydrocarbon-water surface tension as lipids are held together by hydrophobic interactions.
- However biomembranes rupture at a much lower tension. Rupture is a dynamical property and the level of strength depends on the time frame of loading.

# Our objective is to develop a minimal theoretical framework of the DTS method.

## There are two steps :

- First, pore nucleation is described as an activated process following a first order kinetics with a rate  $q$ . It means that the distribution of times for the membrane to remain free of pores is given by the exponential distribution with the rate  $q$ . The pore nucleation rate  $q(\sigma)$  is a function of the membrane surface tension  $\sigma$ .
- Second, based on the Kramers reaction rate theory we describe the pore growth and membrane rupture dynamics as a Markovian stochastic process crossing a time-dependent energy barrier.

# Pore diffusion

- Once the pore is already formed, the net energy  $V(r)$  of such a membrane of thickness  $l$

$$V(r) = 2\pi\gamma r - \pi\sigma r^2$$

- The surface tension  $\sigma$  favoring the pore expansion, and energy cost  $\gamma$  of forming a pore edge (line tension) favoring the closure.
- Assuming  $\sigma > 0$  and  $\gamma > 0$  and both are constant,  $V(r)$  predicts :

$$a = \frac{\gamma}{\sigma}$$

where  $a$  is the pore radius for the maximum energy  $V(r)$ .

- If  $r < a$  the radial force tends to reseal the pore and the membrane remains stable against pore growth.
- However if  $r > a$  a pore will grow without bound and, ultimately, will rupture the membrane.

# Pore diffusion for DTS technique

- $\gamma$  remains constant but

$$\sigma = \sigma_0 + Ft$$

where  $\sigma_0$  is the unstressed membrane tension and  $F$  is the loading rate constant.

- In this case, the critical radius  $a(t)$  becomes a decreasing of time. Therefore any pore initially with radius  $r < a(0)$  will ultimately lead to membrane rupture at a time such that  $r > a(t)$  as a result of the decreasing of both the critical pore radius and associated barrier energy.
- Incorporating thermal fluctuations we view the rupture of the membrane as a Brownian process crossing the time-dependent energy barrier  $V[a(t)]$ .



# Kramers theory

- Dynamics of a pore radius  $r$  is governed by the Langevin equation with the time dependent potential

$$\zeta \frac{dr}{dt} = -\frac{dV(r, t)}{dr} + f(t)$$

- where

$$V(r, t) = 2\pi\gamma r - \pi(\sigma_0 + Ft)r^2$$

$\zeta = 4\pi\eta_m l$  is the friction coefficient with  $\eta_m$  the internal 2D membrane viscosity, and  $f(t)$  is a Gaussian random force of zero mean with

$$\langle f(t)f(t') \rangle = 2\zeta k_B T \delta(t - t')$$

# Parameters and dimensionless variables. The index "0" denotes quantities for unstressed membrane

Symbols	Definition
$\gamma$	line tension ( <i>energy/length</i> )
$\sigma_0$	unstressed surface tension ( <i>energy/surface</i> )
$F$	tension loading rate ( <i>energy/surface/time</i> )
$D = k_B T / \zeta$	pore diffusion coefficient ( <i>length<sup>2</sup>/time</i> )
$r_0 = \gamma / \sigma_0$	critical pore radius ( <i>length</i> )
$\tau = r_0^2 / D$	diffusing time scale of the critical pore ( <i>time</i> )
$F_0 = \sigma_0 / \tau$	critical tension loading rate ( <i>energy/surface/time</i> )
$q_0$	reduced unstressed pore nucleation rate
$x = r / r_0$	reduced pore radius
$y = \sigma / \sigma_0$	reduced membrane surface tension
$\varepsilon = \pi \gamma^2 / \sigma_0 k_B T$	reduced energy barrier for unstressed membrane
$v = F / F_0$	reduced tension loading rate : $\begin{cases} v < 1 : \text{diffusing limit} \\ v > 1 : \text{drift limit} \end{cases}$

# Dimensionless equations

- In dimensionless variables  $x = r/r_0$ ,  $y = \sigma/\sigma_0$ , and  $t \rightarrow t/\tau$  with  $x \in [0, 1]$  and  $y \in [1, \infty[$ .
- This operation leads us to define the control parameter

$$v = \frac{F\tau}{\sigma_0} \equiv \frac{\text{diffusing time scale}}{\text{surface tension time scale}}.$$

- Two regimes in the dynamics of the membrane rupture : the diffusion-controlled regime  $v \ll 1$  and the drift regime for  $v \gg 1$  limit.
- Then dynamic equations

$$\begin{cases} \frac{dx}{dt} = -\frac{dU(x, y)}{dx} + X(t) \\ \frac{dy}{dt} = v \end{cases}$$

where  $\langle X(t)X(t') \rangle = 2\delta(t - t')$ .

# Potential landscape for DTS

- $$U(x|y) = \frac{\varepsilon}{2}[2x - yx^2]$$

with  $\varepsilon = V(r_0)/(k_B T) = (\pi\gamma^2)/(\sigma_0 k_B T)$ .

- The potential  $U(x|y)$  is maximum at  $x^* = 1/y$  corresponding to the energy barrier  $U^* = U(x^*|y) = \varepsilon/2y$ . Both the position  $x^*$  and height  $U^*$  of the energy barrier decrease as  $y$  becomes larger as a result of the membrane stress.

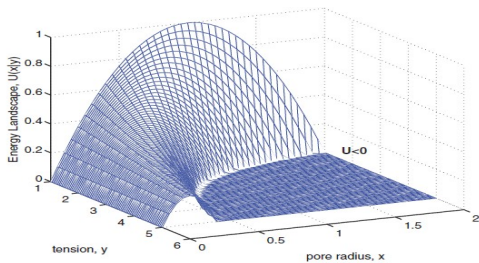


FIG.: Energy landscape with  $\varepsilon = 2$  (flat area  $x > 2/y$  corresponds to  $U < 0$ )

# Our goal

- As the barrier crossing to both pore nucleation and membrane rupture are stochastic processes, both the membrane life time and the membrane tension at rupture are distributed.
- Our goal is to calculate the two quantities that characterize the kinetics of membrane rupture in DTS experiments : the rate of membrane rupture and the distribution of tension at membrane rupture.

# Simplest example

- For a membrane with a pore in the absence of mechanical stress  $v = 0$ , the distribution of tension at membrane rupture is the delta function

$$Q(y) = \delta(y - 1)$$

and the rate of the membrane rupture can be obtained by using the first passage time approach

$$\frac{1}{k(\epsilon|0)} = \int_0^1 \frac{dx}{p_{eq}(x|1)} \left( \int_0^x p_{eq}(z|1) dz \right)^2$$

We assume that the membrane is initially prepared with the distribution  $p_{eq}(x|1)$ , where

$$p_{eq}(x|y) = \frac{\exp(-U(x|y))}{Z(y)}; \quad Z(y) = \int_0^{1/y} \exp(-U(x|y)) dx$$

then  $1/k(\epsilon|0)$  is obtained analytically in terms of the error function  $erf(\dots)$  and  $erfi(z) \equiv erf(iz)/i$ .

# Rate of unstressed membrane rupture

- $$\frac{1}{k(\epsilon|0)} = \frac{\sqrt{\pi/(2\epsilon)}}{\operatorname{erfi}[\sqrt{\epsilon/2}]} \int_0^1 dx \exp(-\epsilon(x-1)^2/2) \\ \times \left\{ \operatorname{erfi}[\sqrt{\epsilon/2}] - \operatorname{erfi}[(1-x)\sqrt{\epsilon/2}] \right\}^2$$



**DIGRESSION to EXPLAIN FIRST PASSAGE TIME APPROACH.**

# First passage time approach

- There are a variety of problems where one wishes to calculate the average time  $\tau_1$  required for a particle, generated at some point and diffusing under the influence of a potential to reach a certain target.  $\tau_1$  is related to the probability  $\Sigma(t)$  that a system is still unreacted at time  $t$

$$\Sigma(t) \simeq \Sigma_{approx}(t) = \exp(-t/\tau_1)$$

- Approximation of a single exponential decay of  $\Sigma(t)$  means that  $\tau_1 = \int_0^\infty dt \Sigma(t)$ .
- $\Sigma(t)$  in turn is related to the distribution  $p(r, t)$  of finding the system at position  $r$  at time  $t$  :  $\Sigma(t) = \int dr p(r, t)$ .
- $p(r, t)$  obeys the Smoluchowski equation

$$\frac{\partial p(r, t)}{\partial t} = \nabla \mathbf{j}(r, t); \mathbf{j}(r, t) = D(r)[\nabla p(r, t) + \beta p(r, t) \nabla U(r)]$$

where  $\mathbf{j}$  is the corresponding flux,  $D(r)$  is the position dependent diffusion coefficient, and  $U(r)$  is an external potential.

# Technical details to the 1-st passage time approach.

- Notations in particle terminology : If the particle was at  $r_0$  at  $t = 0$ , the probability that it has not been absorbed at time  $t$  is

$$\Sigma(r_0, t) = \int dr p(r, t | r_0, 0)$$

and the average time required for adsorption

$$\tau_1(r_0) = \int_0^{\infty} dt \Sigma(r_0, t)$$

- Instead of solving the equation for  $p(r, t | r_0, 0)$  and then integrating over  $r$  to obtain  $\Sigma(r_0, t)$  one can derive a differential equation which determines  $\Sigma(r_0, t)$  directly.
- The adjoint to Smoluchowski equation which holds for the adjoint operator

$$L^* = \nabla D(r) \nabla - \beta D(r) (\nabla U) \nabla$$

## Technical details (continuation)

- The differential equation for  $\Sigma(r_0, t)$  (L.Pontryagin, JETP, 1933)

$$\frac{\partial \Sigma(r_0, t)}{\partial t} = L^*(r_0)\Sigma(r_0, t)$$

- Then differential equation for  $\tau_1(r_0)$  by virtue  $\int_0^\infty dt(\partial/\partial t)\Sigma(r_0, t) = -1$

$$L^*(r_0)\tau_1(r_0) = -1$$

- The first passage time theory addresses the case of the Smoluchowski boundary condition for which every encounter at  $r = a$  leads to reaction, making  $\tau_1(r_0)$  the average time required to reach  $r = a$  for the 1-st time starting from  $r = r_0$ . We enclose our system and prevent any particles from escaping by erecting a reflective barrier at  $r = 0$  ( $j(0, t) = 0$ ).
- While this equation is general, it can be solved analytically only when boundary conditions, the potential, and the diffusion coefficient depend solely on a single coordinate.

**Back to DTS in membranes.**

# DTS observables for a stressed membrane

- For a membrane initially free of pore but stressed  $v > 0$  the rate of membrane rupture and the distribution of tension at membrane rupture can be determined in terms of the survival probability  $\Sigma(t)$ . The membrane rupture rate  $k(\epsilon|v)$  (inverse of the membrane lifetime)

$$\frac{1}{k(\epsilon|v)} = \int_0^{\infty} t \left( -\frac{d\Sigma(t)}{dt} \right) dt = \int_0^{\infty} \Sigma(t) dt$$

- Likewise, the distribution  $Q(y)$  of tensions  $y$  at which membrane rupture is related to the distribution of rupture time and, as  $y = 1 + vt$

$$Q(y) = \left| \frac{dt}{dy} \right| \left( -\frac{d\Sigma}{dt} \right)_{y=1+vt}$$

# Survival probability to describe membrane fate

- The DTS spectrum for rupture tensions

$$\langle y(\epsilon|v) \rangle = \int_1^\infty yQ(y)dy$$

and it is related to the rupture rate by

$$\langle y(\epsilon|v) \rangle = 1 + \frac{v}{k(\epsilon|v)}$$

- In the case  $\Sigma(t)$  satisfies a 1st order rate equation with the effective time dependent rate  $\Gamma(t)$  (not the same as the bare function  $q(t)$ ), i.e.,  $\Sigma(t) = \exp(-\int_0^t \Gamma(t')dt')$ , the distribution  $Q(y)$

$$Q(y) = \frac{\Gamma((y-1)/v)}{v} \exp \left[ - \int_0^{(y-1)/v} \Gamma(z)dz \right]$$

Thus  $\Sigma(t)$  is the key function to find !

# Analytical theory

- Instead of stochastic equations for  $x$  and  $y$  one can write Fokker-Planck equation for the joint probability density  $P(x, y, t)$

$$\frac{\partial P(x, y, t)}{\partial t} = -v \frac{\partial P(x, y, t)}{\partial y} - \frac{\partial J(x, y, t)}{\partial x}$$

where the 1st term in the rhs -ballistic drift caused by the applied loading rate, and the 2d term is the diffusive flux for a given  $y$

$$J(x, y, t) = - \exp(-U(x|y)) \frac{\partial}{\partial x} \exp(U(x|y)) P(x, y, t)$$

it reduces to Smoluchowski equation for  $v = 0$ .

- $P(x, y, t)$  satisfies the reflecting boundary condition at  $x = 0$  and the adsorbing boundary condition at  $x = 1/y$  :

$$J(x, y, t) = 0 \quad x = 0; \quad P(x, y, t) = 0 \quad x = 1/y$$

and initial condition  $P(x, y, t = t_0 | x_0, y_0) = \delta(x - x_0) \delta(y - y_0)$ .



# Formal, yet numerically computable solution

- Green's function

$$P(x, y, t|x_0, y_0, t_0) = \left( \frac{\rho_{eq}(x|y)}{\rho_{eq}(x_0|y_0)} \right)^{1/2} \delta[y - y_0 - v(t - t_0)] \\ \times \sum_{n=1}^{\infty} \psi_n(x_0|y_0) \psi_n(x|y) \exp[-(1/v) \int_{y_0}^y \lambda_n(z) dz]$$

where  $\psi_n(x|y)$  and  $\lambda_n(y)$  are normalized eigenfunctions

$\int_0^{1/y} dx \psi_n(x) \psi_{n'}(x) = \delta_{n,n'}$  and eigenvalues for the Hamiltonian

$$H\psi = \frac{d^2\psi}{dx^2} - \left[ \frac{v\epsilon x^2}{4} + \frac{\epsilon^2(1-yx)^2}{4} + \frac{\epsilon y}{2} \right] \psi = -\lambda\psi$$

- satisfying the reflecting and absorbing boundary conditions at  $x = 0$  and  $x = 1/y$

$$\exp(-U(x)) \frac{\partial}{\partial x} [\exp(U(x)/2) \psi(x)]_{x=0} = 0; \psi(x = 1/y) = 0$$

# Change of variables

- Let  $z = (v\epsilon + \epsilon^2 y^2)^{1/4} (x - \epsilon y / (v + \epsilon y^2))$  with  $z_0 \leq z \leq z_1$ , where

$$z_0 = -\frac{\epsilon y (v\epsilon + \epsilon^2 y^2)^{1/4}}{(v + \epsilon y^2)} ; z_1 = \frac{v (v\epsilon + \epsilon^2 y^2)^{1/4}}{y (v + \epsilon y^2)}$$

- Then the equation  $H\psi = -\lambda\psi$

$$\frac{d^2\psi}{dz^2} - \left[ E - \frac{z^2}{4} \right] = 0$$

where

$$E = \frac{1}{(v\epsilon + \epsilon^2 y^2)^{1/2}} \left( \lambda - \left( \frac{\epsilon y}{2} + \frac{v\epsilon^2}{4(v + \epsilon y^2)} \right) \right)$$

# Formal solution (continuation)

- The general solution satisfying the reflecting and absorbing boundary conditions

$$\psi(z) = A[D_\nu(-z_1)D_\nu(z) - D_\nu(z_1)D_\nu(-z)]; \nu = E - \frac{1}{2}$$

where  $D_\nu$  is the Weber (parabolic cylinder) function.

- $A$  is obtained from the normalization, and the eigenvalue by using BC

$$D_\nu(-z_1) \left( \frac{dD_\nu(z_0)}{dz_0} + \frac{\epsilon}{2(\nu\epsilon + \epsilon^2 y^2)^{1/4}} D_\nu(z_0) \right) \\ + D_\nu(z_1) \left( \frac{dD_\nu(z_1)}{dz_0} - \frac{\epsilon}{2[\nu\epsilon + \epsilon^2 y^2]^{1/4}} D_\nu(-z_0) \right) = 0$$

# Last efforts

- Assuming that the system is initially prepared with the distribution function  $g(x, y, t)$ , then

$$\Sigma(t) = \int_1^\infty dy_0 \int_1^\infty dy \int_0^{1/y_0} dx_0 \int_0^t dt_0 P(x, y, t | x_0, y_0, t_0) g(x_0, y_0, t_0)$$

where

$$g(x, y, t) = p_{eq}(x|y) \delta(y - 1 - vt) \left[ q(t) \exp \left( - \int_0^t q(t') dt' \right) \right]$$

and the term [...] stands for the distribution of times for pore nucleation.

- This is exact expression of  $\Sigma(t)$  from which the rupture rate  $k(\epsilon|v)$  (the DTS spectrum), and the distribution  $Q(y)$  of rupture tension and also time dependent rate  $\Gamma(t)$  can be found. Unfortunately, the derivation is very tedious, and analytical expressions unpractical for explicit calculations.

# OUR RESULTS.

# Distribution $Q(y)$ of rupture tensions $y$

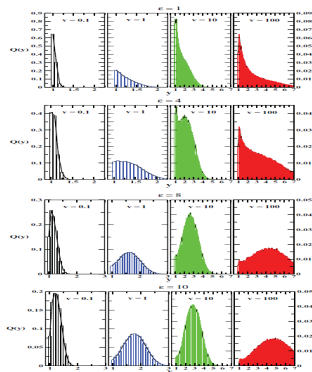


FIG.:  $q(y) = q_0 \exp(\alpha(y - 1))$  with  $q_0 = 0.1$  and  $\alpha = 1$ .

# DTS spectrum $\langle y(\epsilon|v) \rangle$ as a function of the barrier height $\epsilon$

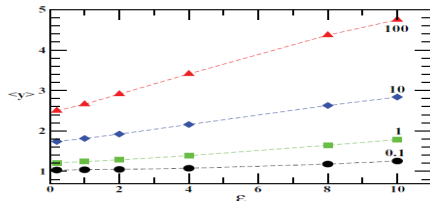


FIG.: Loading rates  $v$  are quoted numbers

# DTS spectrum $\langle y(\epsilon|v) \rangle$ as a function of the loading rate $v$

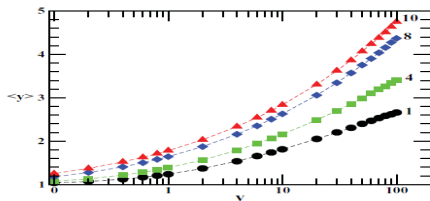


FIG.: Barrier heights  $\epsilon$  are quoted numbers.



# $Q(y)$ for various tension independent pore nucleation rate $q_0$

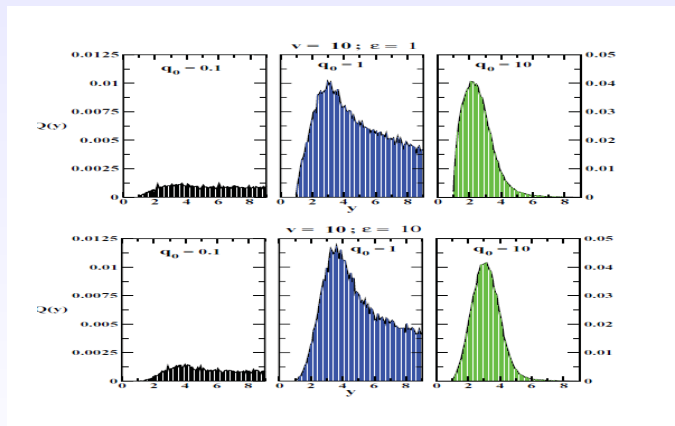


FIG.:  $\alpha = 0$